

Micro-scale damage from cyclic bending loads observed in UD Basalt/Epoxy composites

Ulrich A. Mortensen

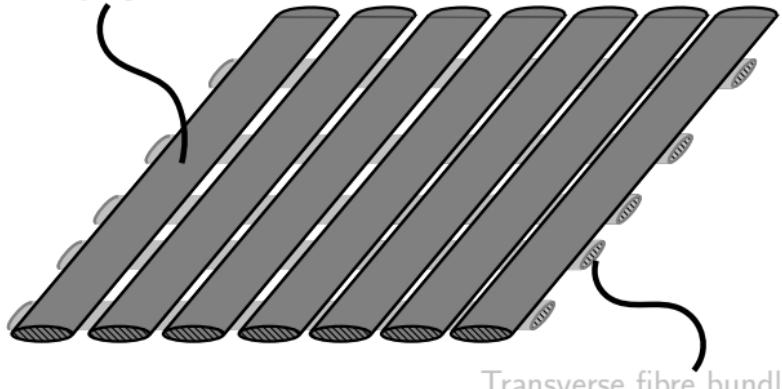
Technical University of Denmark

Department of Wind Energy , Section of Composites & Materials Mechanics

$$P = \frac{1}{2} \rho A v^3 C_p$$

Fibre architecture of Non-crimp fabric

Load Carrying fibre bundles



Top side - Longitudinal



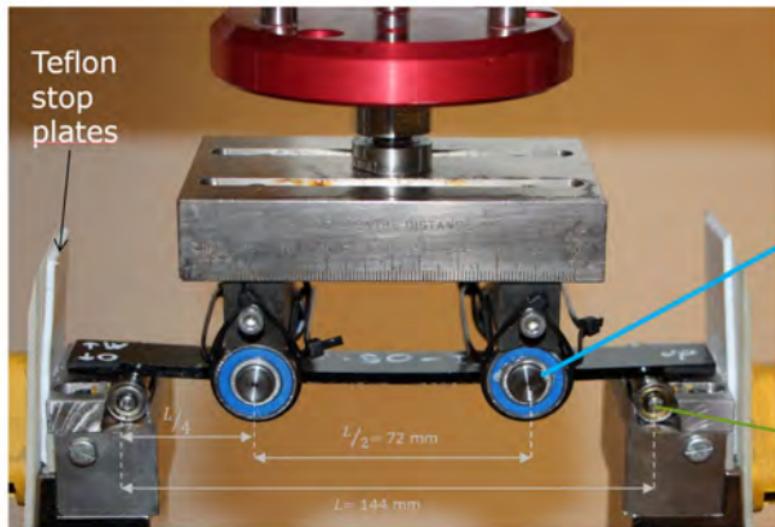
Bottom side - Transverse



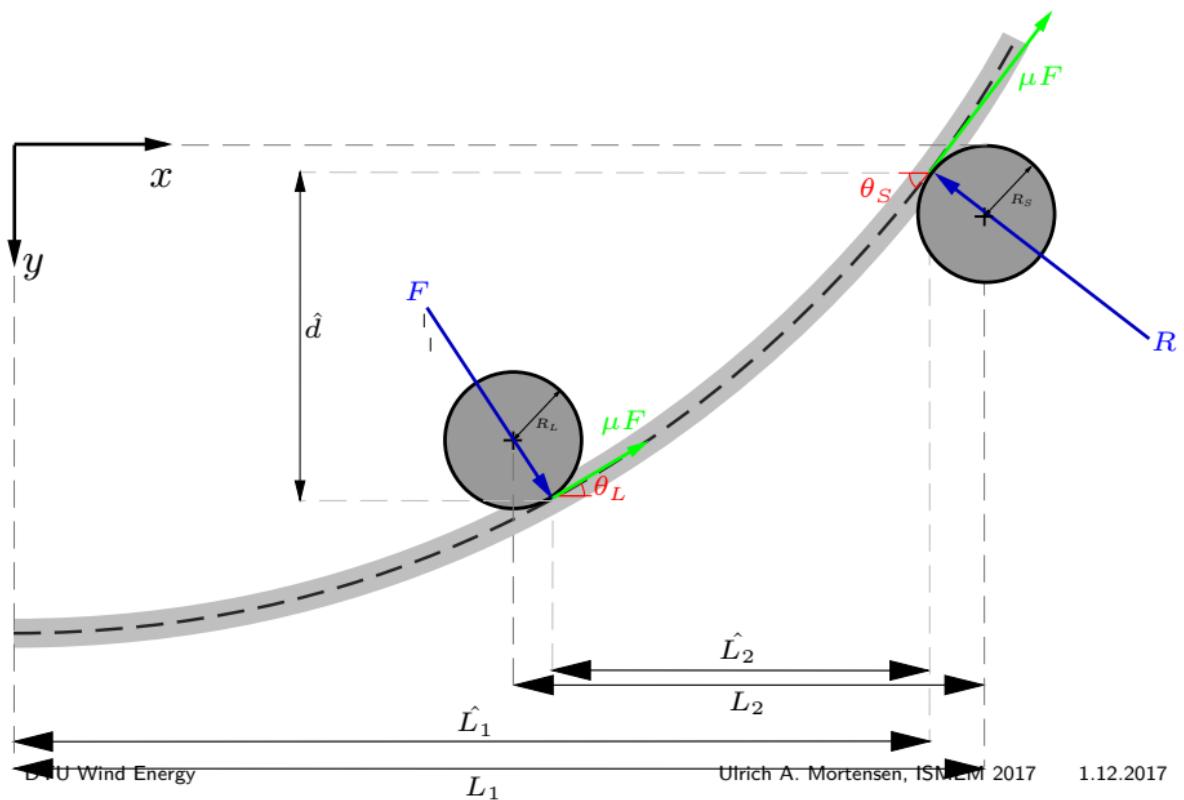
- Transverse (backing bundles and sewing thread) bundles are needed for handling (also in Wind Turbine Industry)

Specimen Scale

Set-up and specimen shape



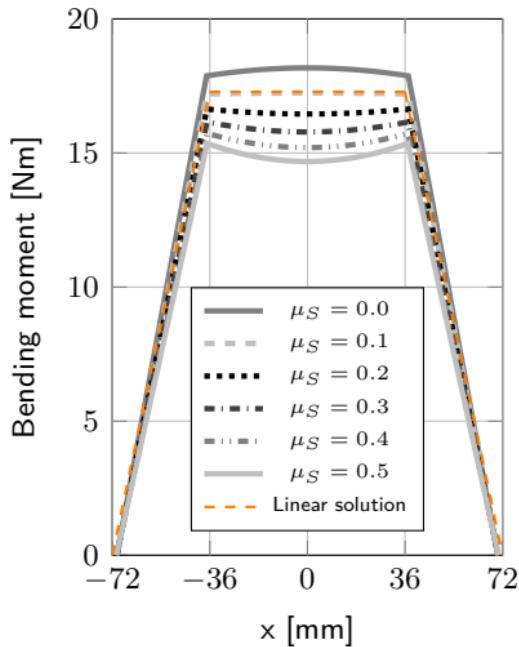
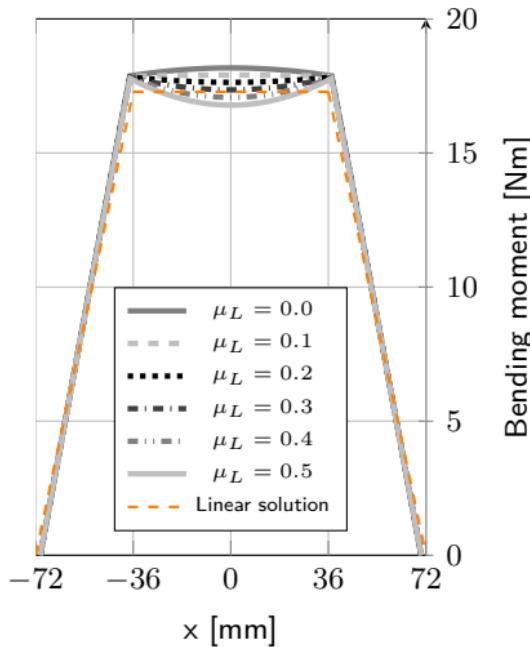
Friction effects on the bending moment - I



$$M = \frac{P}{2} \left[\hat{L}_1 - x + y \underbrace{\frac{\tan \theta_s - \mu_s}{1 + \mu_s \tan \theta_s}}_{\text{Non-linear term}} \right] \quad \text{for } x \in [\hat{L}_1 - \hat{L}_2 ; \hat{L}_1] \quad (1)$$

$$M = \frac{P}{2} \left[\hat{L}_2 + y \underbrace{\frac{\tan \theta_s - \mu_s}{1 + \mu_s \tan \theta_s} - (y - \hat{d}) \frac{\tan \theta_L + \mu_L}{1 - \mu_L \tan \theta_L}}_{\text{Non-linear terms}} \right] \quad \text{for } x \in [0 ; \hat{L}_1 - \hat{L}_2] \quad (2)$$

Friction effects on the bending moment - III

(a) $\mu_S \in [0.0; 0.5]$ and $\mu_L = 0.0$ (b) $\mu_L \in [0.0; 0.5]$ and $\mu_S = 0.0$

Specimen Scale S-N Curve

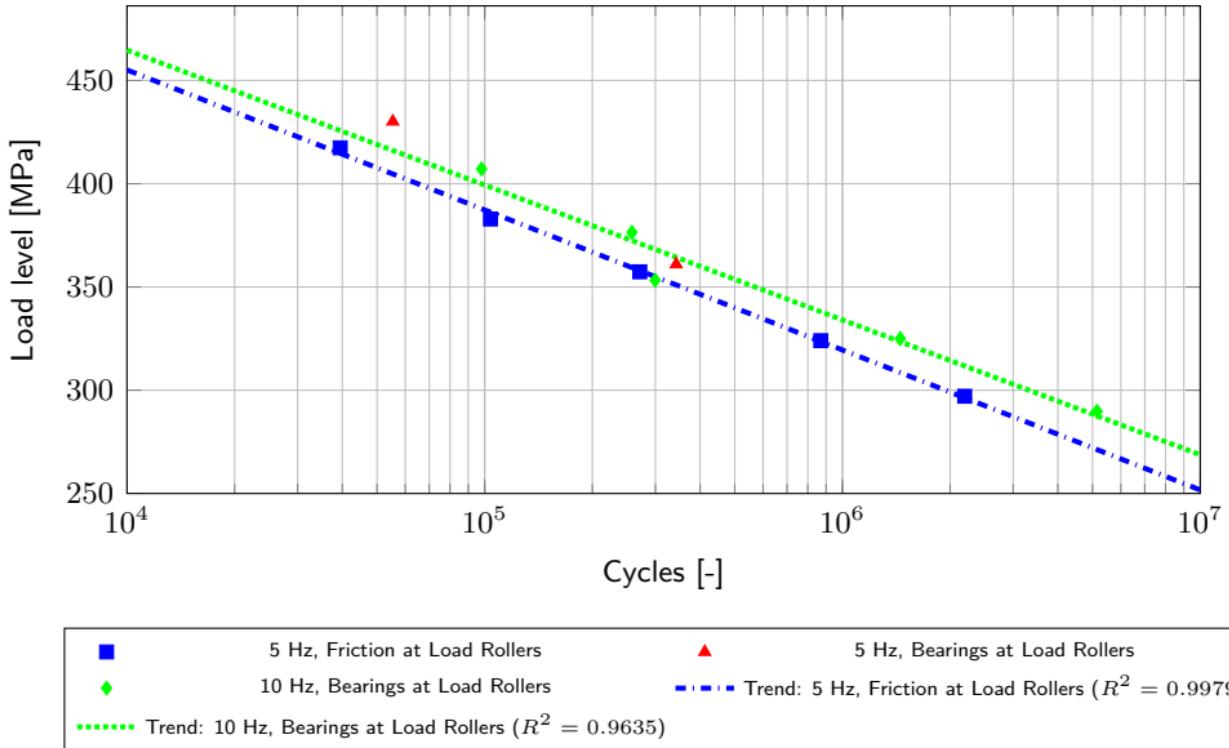
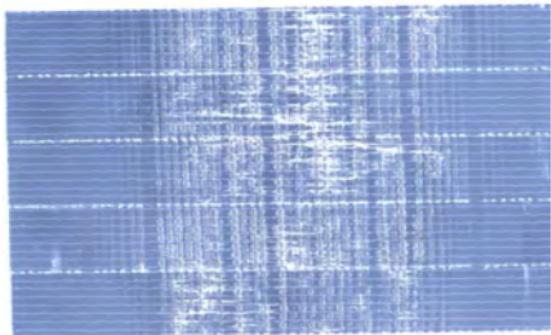


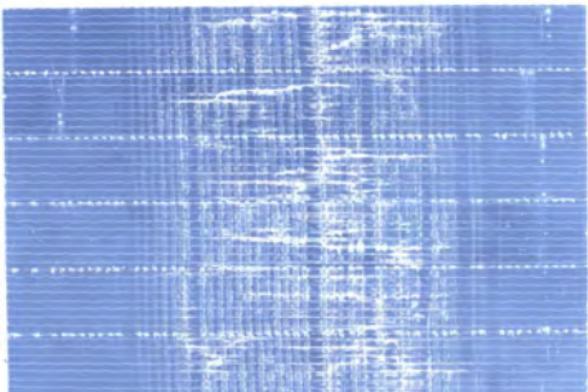


Figure Removed. Will Be
available in paper to be
published in 2018

Macro scale damage due to patterns of transverse fibre bundles



(a) Batch A, small friction at load rollers



(b) Batch B, No friction at load rollers



Figure: Large Field of View Microscopy. 28 mm by 3.6 mm captured with 700-800 images.

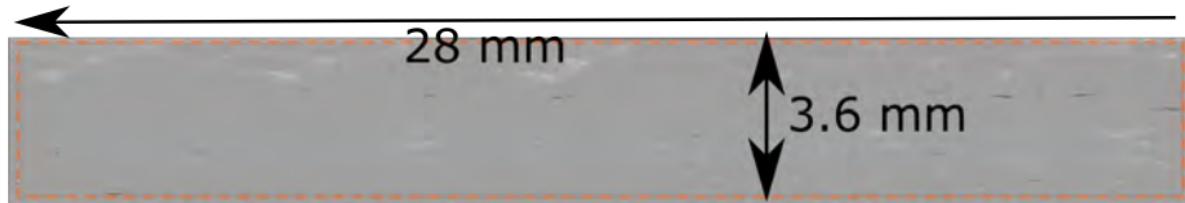


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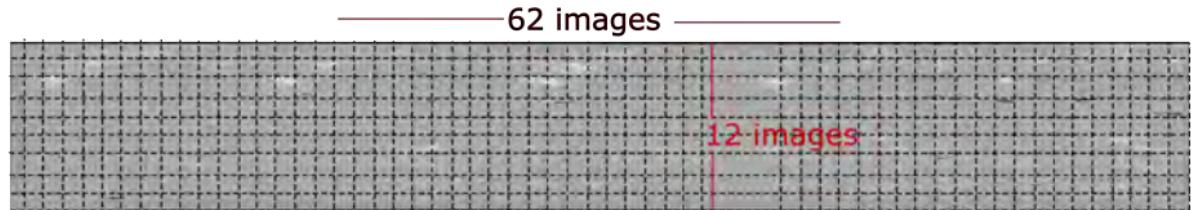


Figure: Large Field of View Microscopy. 28 mm by 3.6 mm captured with 700-800 images.

Examples of micro-scale matrix cracks and fibre breaks

← Loading direction →

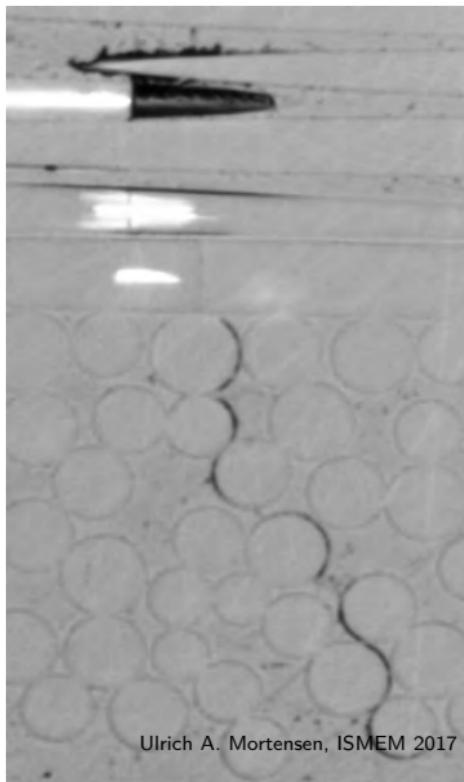
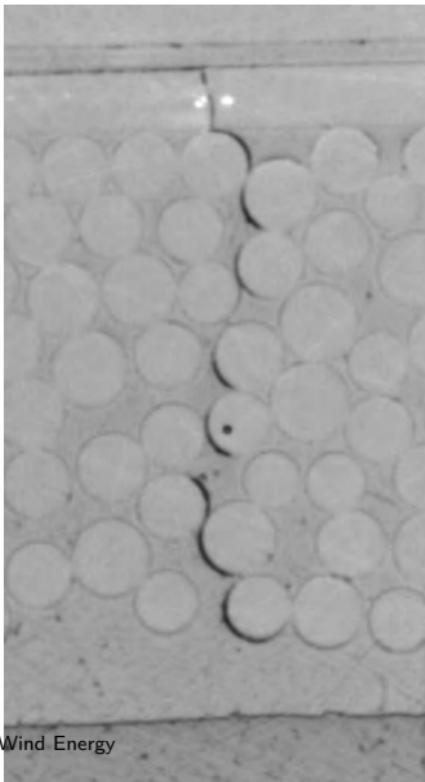
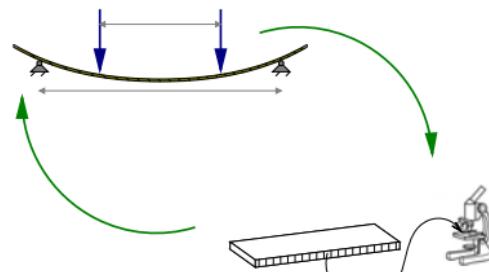




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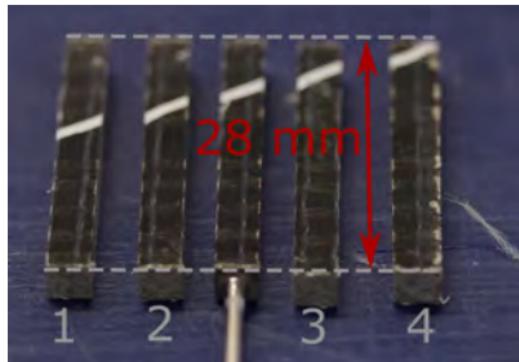
Examples of micro-scale matrix cracks and fibre breaks 2

- Size: 9.7 mm by 3.6 mm, 386 images stitched together
- $[1 - 15] \cdot 10^3$ with 10^3 cycles per interval
- $[15 - 95] \cdot 10^3$ with 10^3 cycles per interval
- $[15 - 95] \cdot 10^3$ with 10^3 cycles per interval
- $[95 - 225] \cdot 10^3$ with $25 \cdot 10^3$ cycles per interval
- $[225 - 1225] \cdot 10^3$ with $250 \cdot 10^3$ cycles per interval

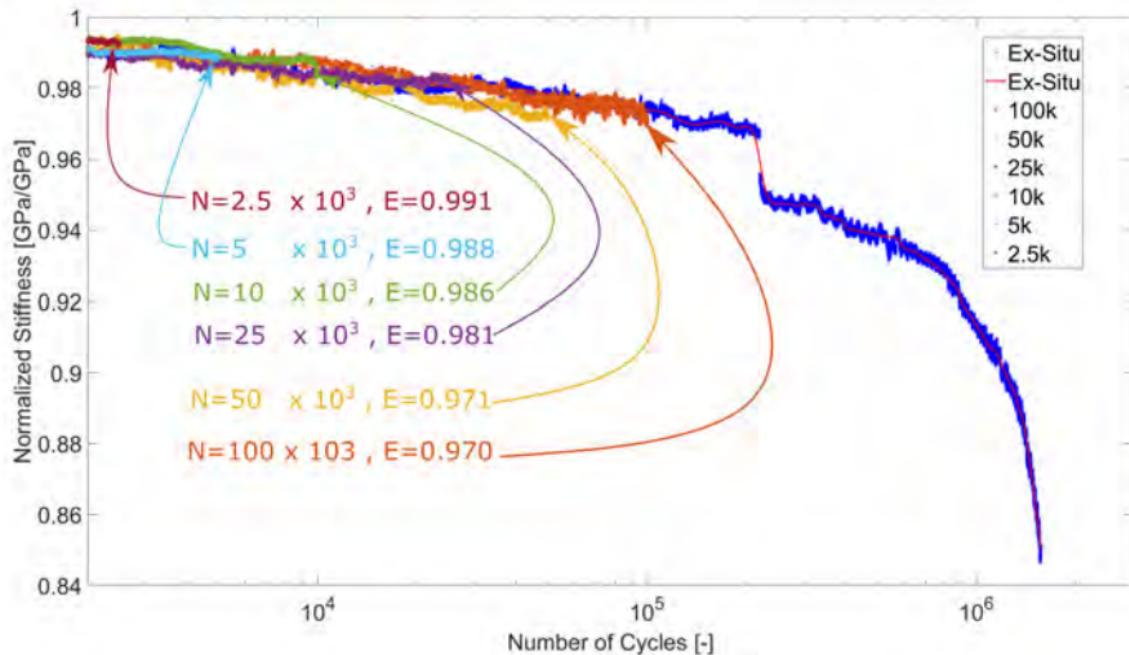


Destructive Microscopy Test

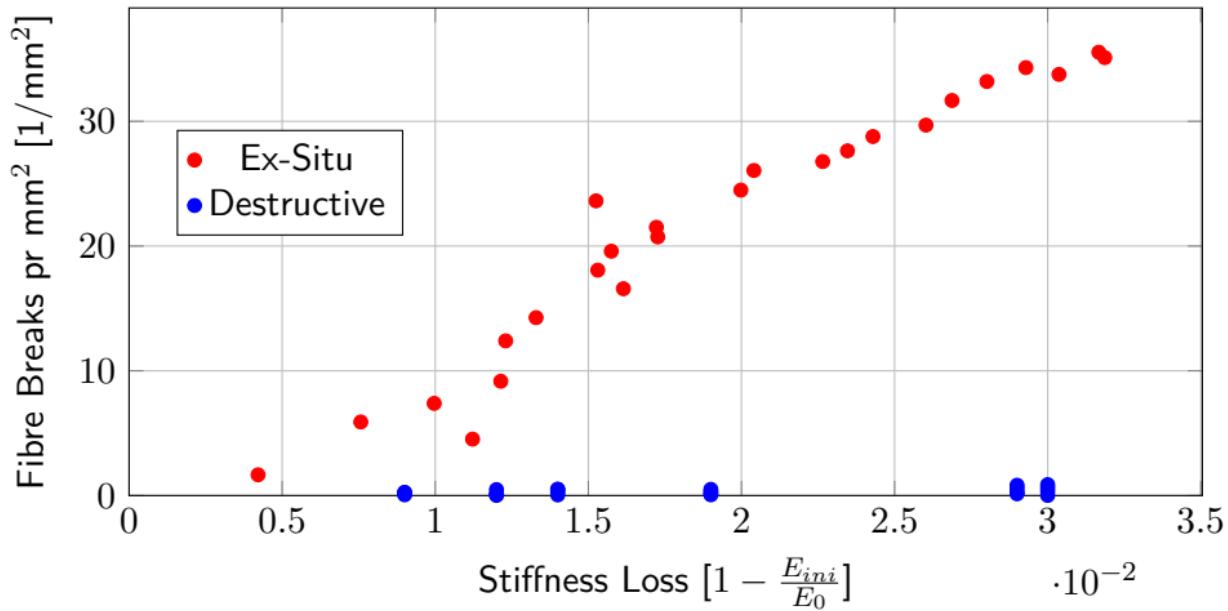
- Six specimens cut adjacent to each other
- All loaded with 325 MPa maximum stress at surfaces
- No. of loadings $N = [2.5, 5, 10, 25, 50, 100] \cdot 10^3$



Stiffness Degradation



Fibre Break Density



Distances from Fibre breaks to Transverse fibre bundles - Ex-Situ - $N = 10 \cdot 10^3$

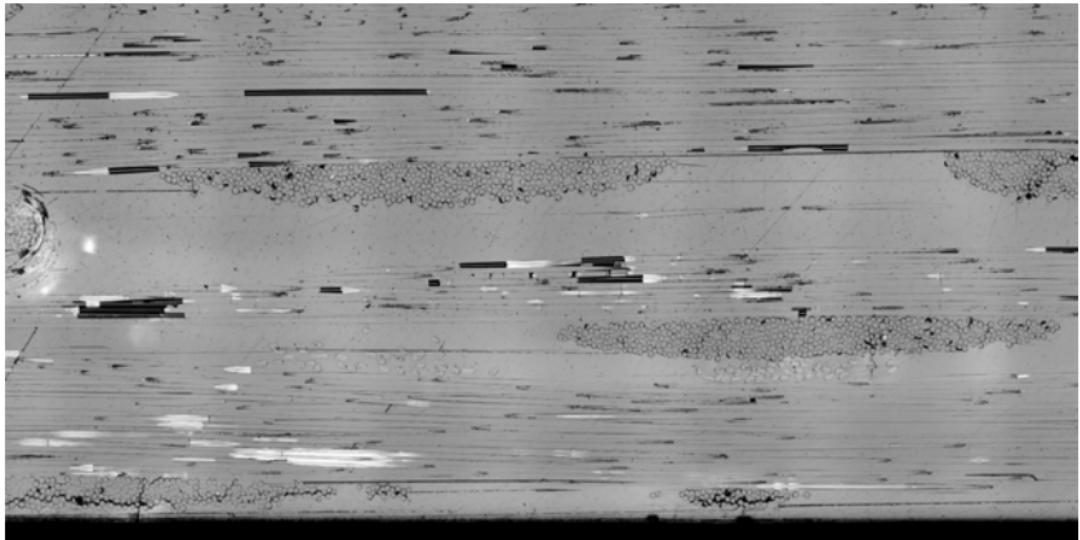


Figure: Fibre break positions in Ex-Situ study

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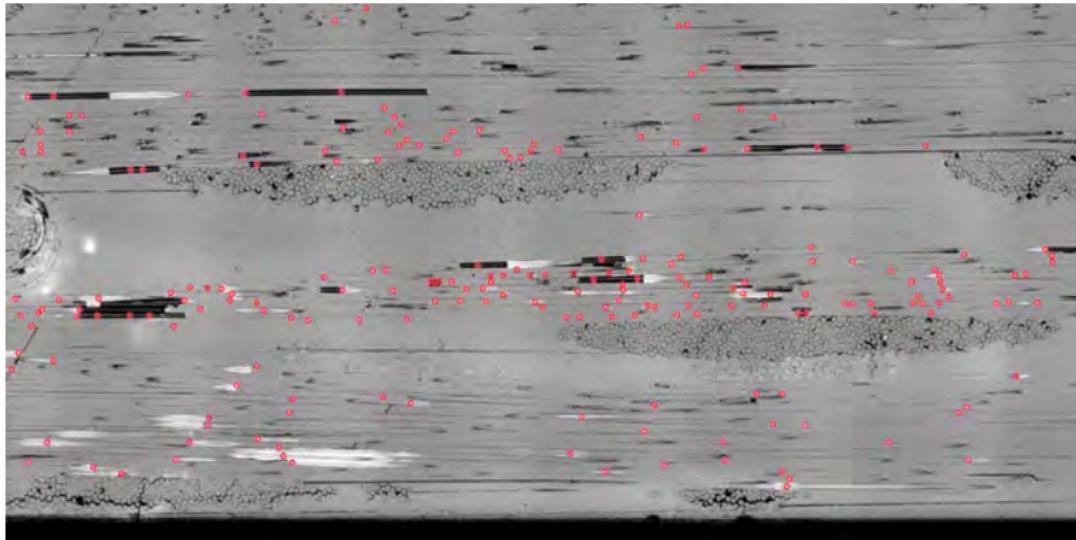


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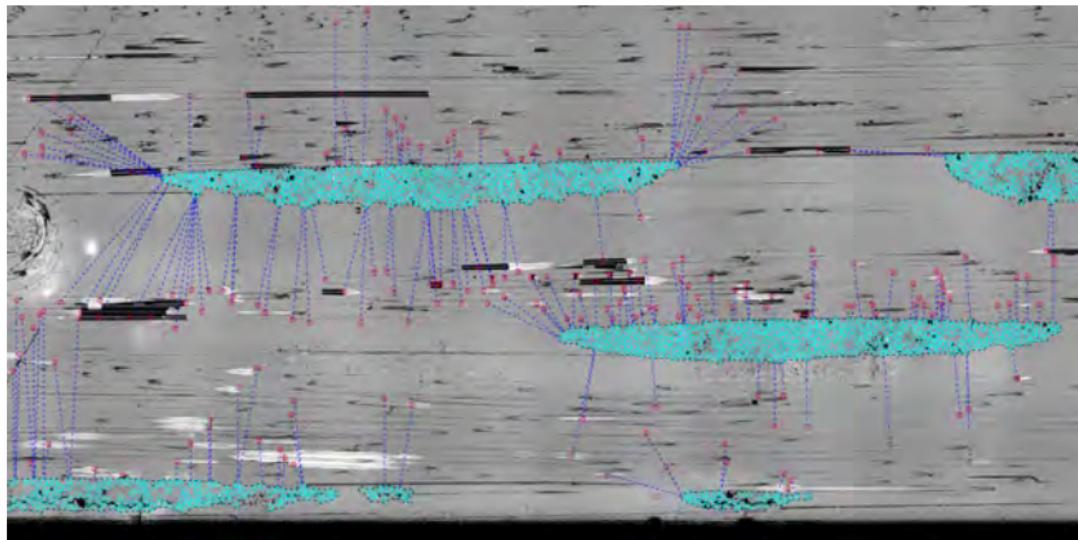


Figure: Fibre break positions in Ex-Situ study

Distances from Fibre breaks to Transverse fibre bundles - Destructive test - $N = 10 \cdot 10^3$

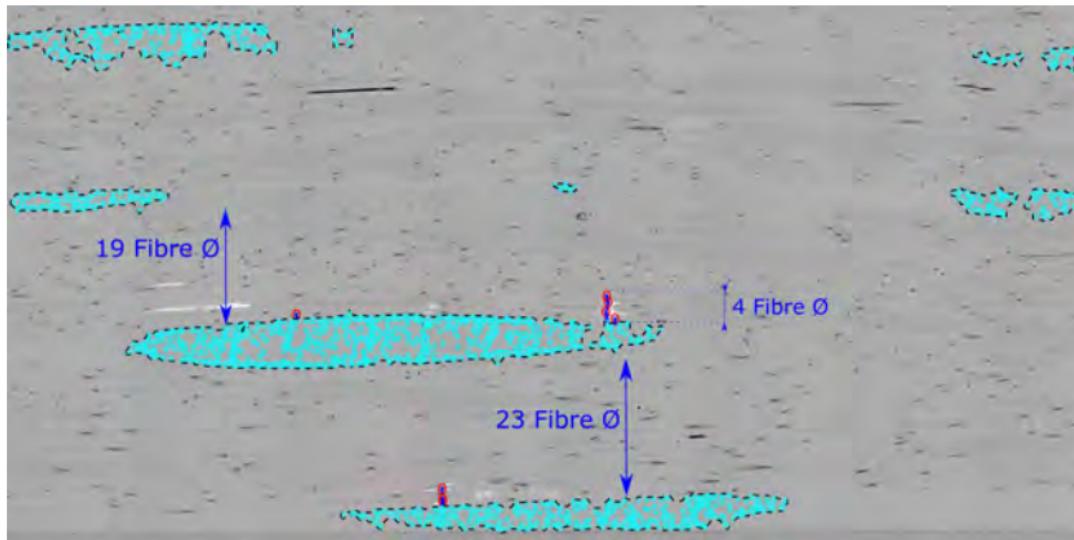
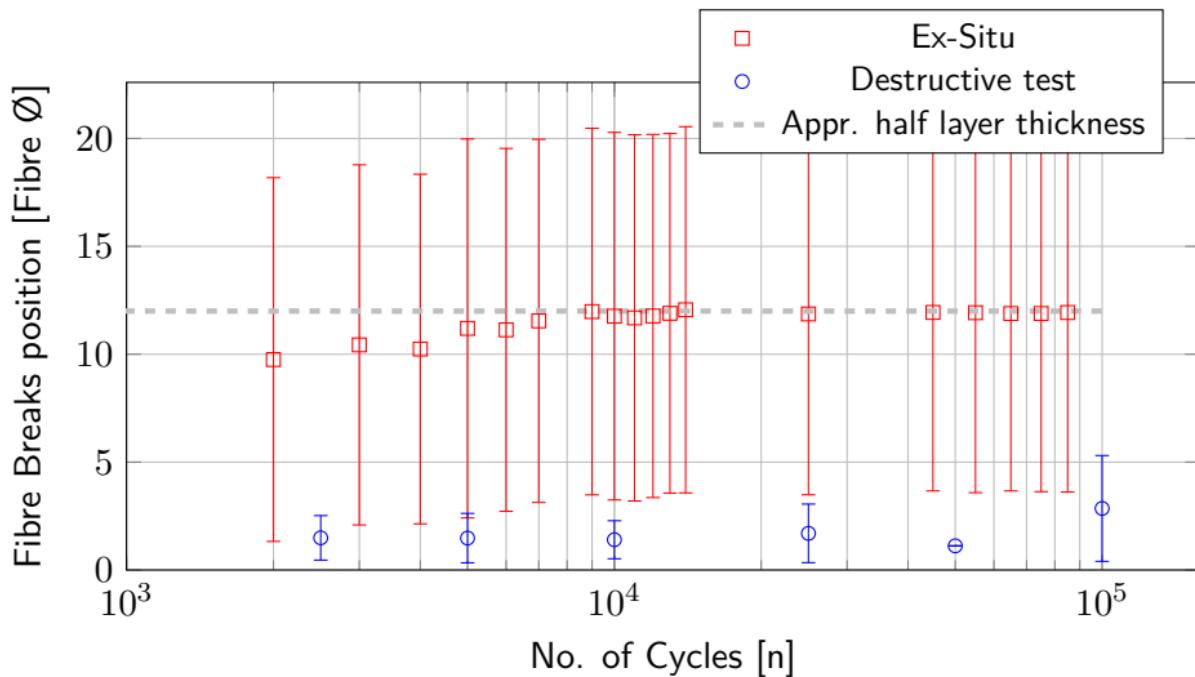


Figure: Fibre break positions in Destructive testing

Fibre Break Density



Conclusion

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- Edge-effects makes Ex-situ study microscopy studies quantitatively unreliable, but may give some qualitative insight into damage mechanisms
- Transverse Matrix cracks in transverse fibre bundles are the main driver for breakage of fibres in the load carrying fibre bundles in uni-directional non-crimp glass fibre fabric.

Thank You!